

# Rotating Circuit Board Probes for Magnetic Measurements

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IMMW15

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# Introduction

Circuit Board Probes – an appealing concept –

- Accurate trace locations
- Manufacture probes reproducibly, cheaply, quickly.

Development at FNAL

- Circuit board trace configurations with **bucking** of fundamental fields (to ease dynamic range requirements and reduce feed-up from vibration effects)
- Designs which have **comparable sensitivity** with standard rotating coil probes.
- **Analysis** which can deal with it

# Generalized Rotating Probe Harmonics Analysis

Dealing with complex or non-ideal rotating harmonics probes is straightforward

Measure  $\phi(\theta) = \Re \sum_{n=1} C_n K_n e^{(in\theta)}$

Field  $C_n = B_n + iA_n$

Any number of wires

Any positions

Probe Sensitivity

$$K_n = \sum_{j=1}^{N_{wires}} \frac{L_n R}{n} \left( \frac{(x_j + iy_j)}{R} \right)^n (-1)^{j+1}$$

Wire polarity sign

Complex conjugate of  $\phi(\theta)$  FFT

$$C_n = \frac{F_n^*}{K_n}$$

Use FFT of rotating probe signal and calculated sensitivities to find Fields

Applicable to all rotating coil data systems

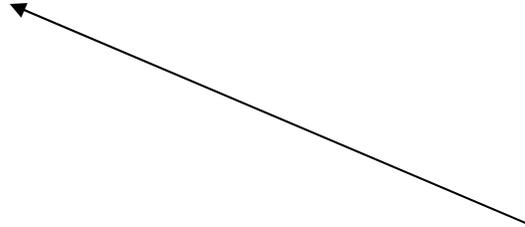
# Probe Parameter Files for Wire Locations

#####

Length(m)	NTURNS	Radius(m)	Phi(rad)
WINDING TAN1			
0.81788	15	0.019539	0.541068
0.81788	15	0.019539	0.768448
WINDING 2P1			
0.830275	1	0.019617	4.81057
0.830275	1	0.019617	1.66898
WINDING 2P2			
0.827126	1	0.019603	-0.359452
0.827126	1	0.019603	2.78215
WINDING 4P1			
0.820725	1	0.019628	-0.414082
0.820725	1	0.019628	1.15672
0.820725	1	0.019628	2.72752
0.820725	1	0.019628	4.29832
WINDING 4P2			
0.823925	1	0.019595	0.152808
0.823925	1	0.019595	1.72361
0.823925	1	0.019595	3.2944
0.823925	1	0.019595	4.8652

Sample parameter  
file for tangential  
probe.

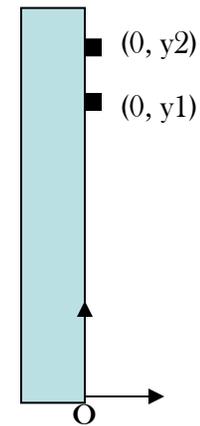
File is read-in and  $K_n$   
calculated for  $n=1-15$   
for each winding



Rows alternate '+'  
and '-' vertices.

# A Simple Circuit Board Probe

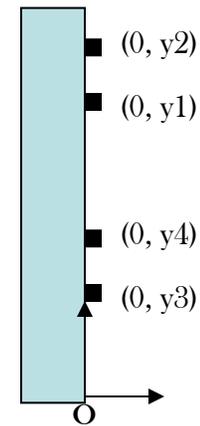
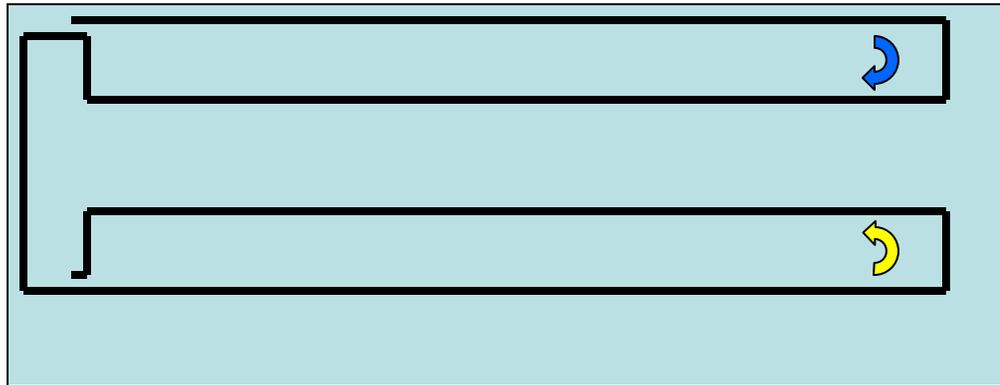
- Radial coil in a plane



$$K_n = \frac{R}{n} \left( L_1 (iy_1)^n - L_2 (iy_2)^n \right)$$

# Dipole Bucked Probe

- Combine 2 simple coils with opposite handedness -  $n=1$  term bucks

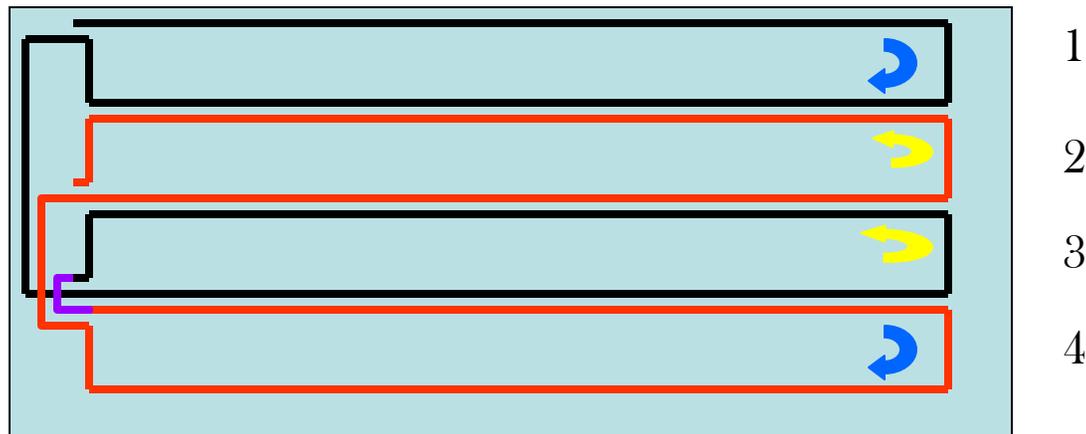


$$K_n = \frac{R}{n} (L_1 (iy_1)^n - L_2 (iy_2)^n) - \frac{R}{n} (L_3 (iy_3)^n - L_4 (iy_4)^n)$$

Still sensitive to other orders - other terms don't buck  
because of radial dependence on powers of  $n$

# Dipole Quad Bucking

- Combine 2 dipole buck pairs with opposite handedness -  
n=1,2 terms bucks

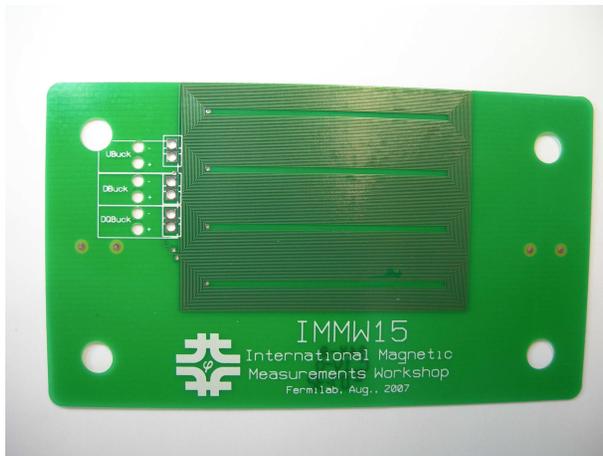


Loops 1,3 buck dipole, as do loops 2,4

Since 1,3 measures gradient and so does 2,4, bucking these two pairs bucks both dipole and quadrupole.

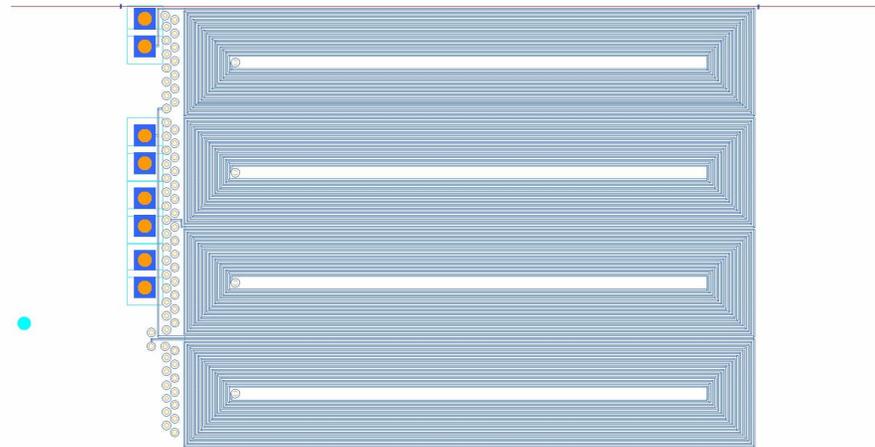
# 39mm DQ Bucking HFQ Probe

2-layer "IMMW" version



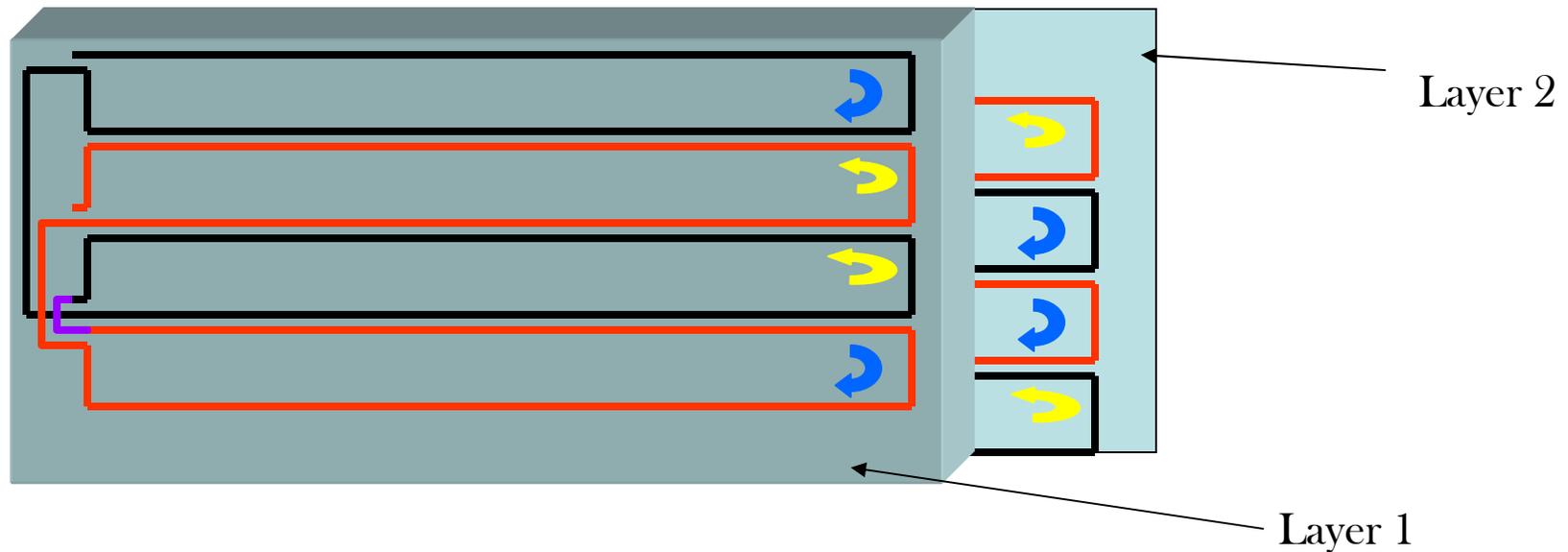
18 turns per loop  
0.1mm space/trace  
39mm effective length

30-layer version  
(note extra via holes for  
interlayer connections)



# Dipole Quad Sextupole Bucking

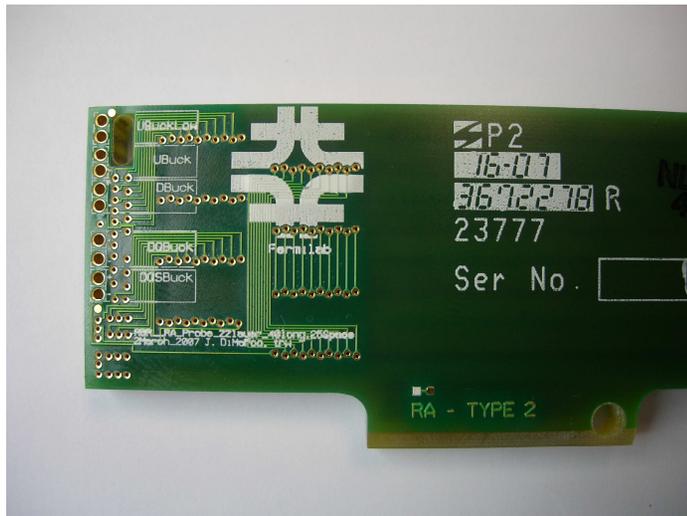
- Combine 2 DQ buck layers with opposite handedness (and offset from each other)  $\rightarrow$   $n=1,2,3$  terms buck



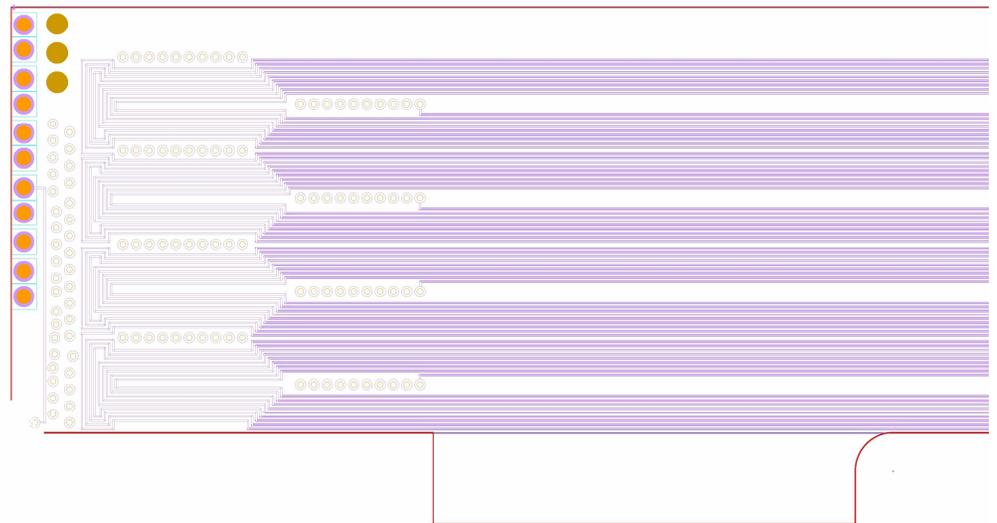
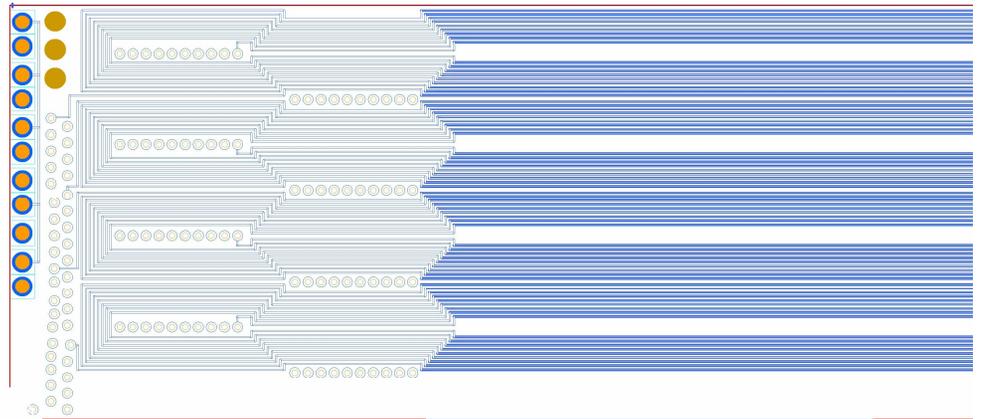
Combined layer 1 loops buck dipole-quad, as do layer 2 loops.

Since layers 1, 2 measure gradient difference (sextupole),  
bucking these two layers bucks sextupole in addition to dipole and quadrupole.

# DQS Bucking Probe for BMA Fixed Coil Measurements



9 turns per loop  
0.15mm/0.1mm space/trace  
1m (40") length





# mechanics

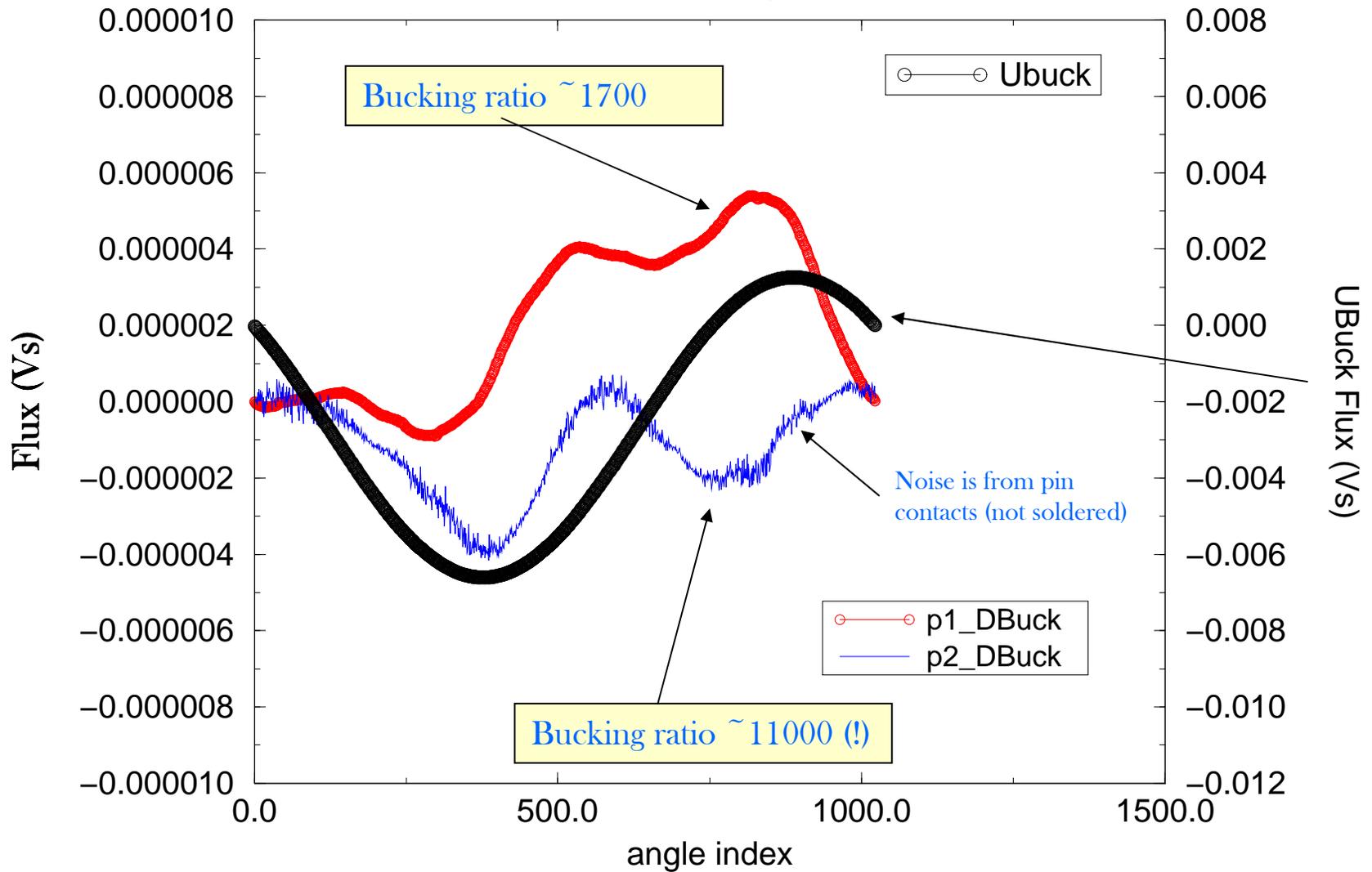
- Using probes themselves as support
- Using cylinder diameter
- Using cylinder radius
- Having probe sticking through slot to maximize radius



# Buck ratio in Dipole (2 probes)

## Probe signals

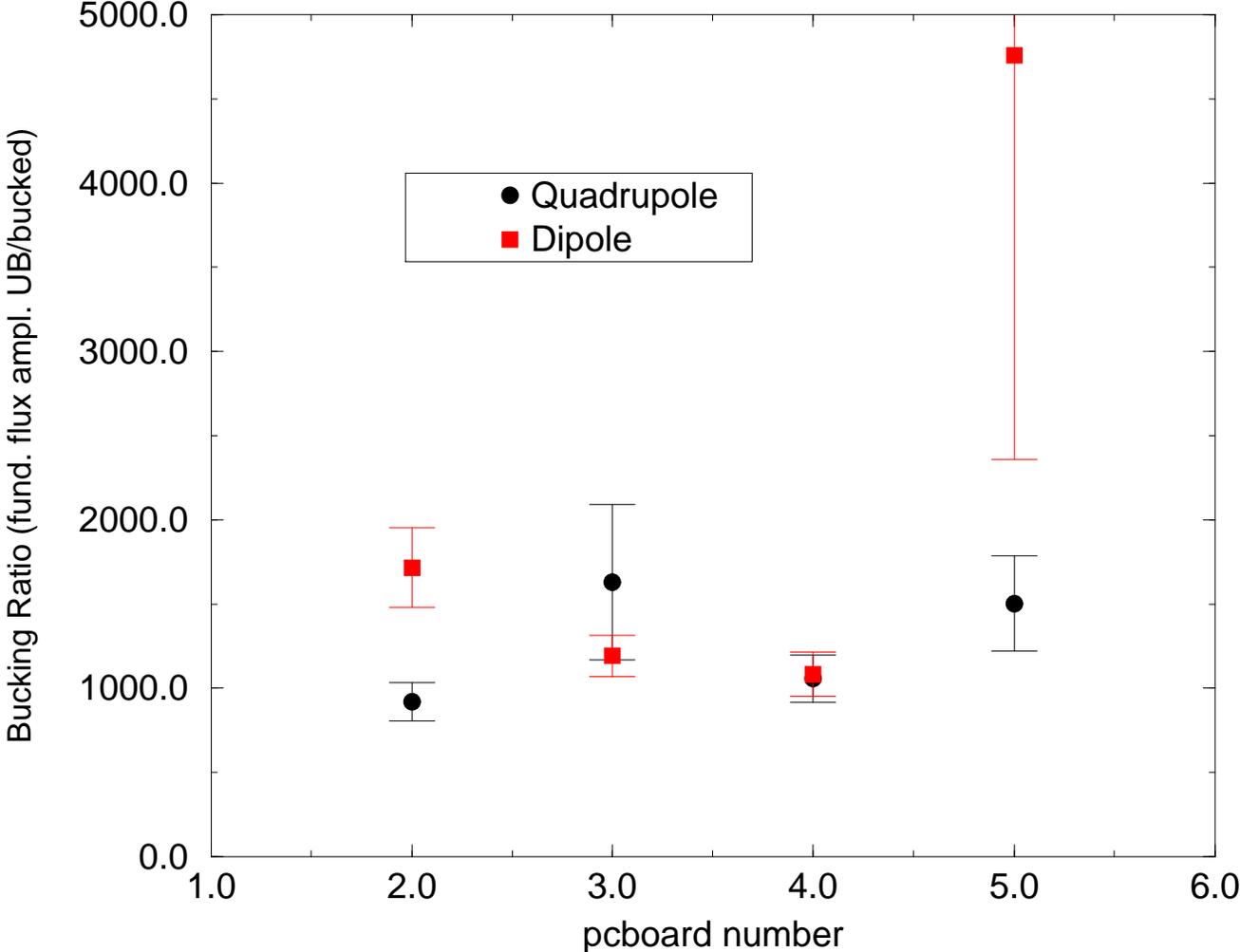
file: rbr\_v3\_dip.dat



# Dipole and Quad buck ratios

## PCboard Bucking Ratios

4 prototype boards

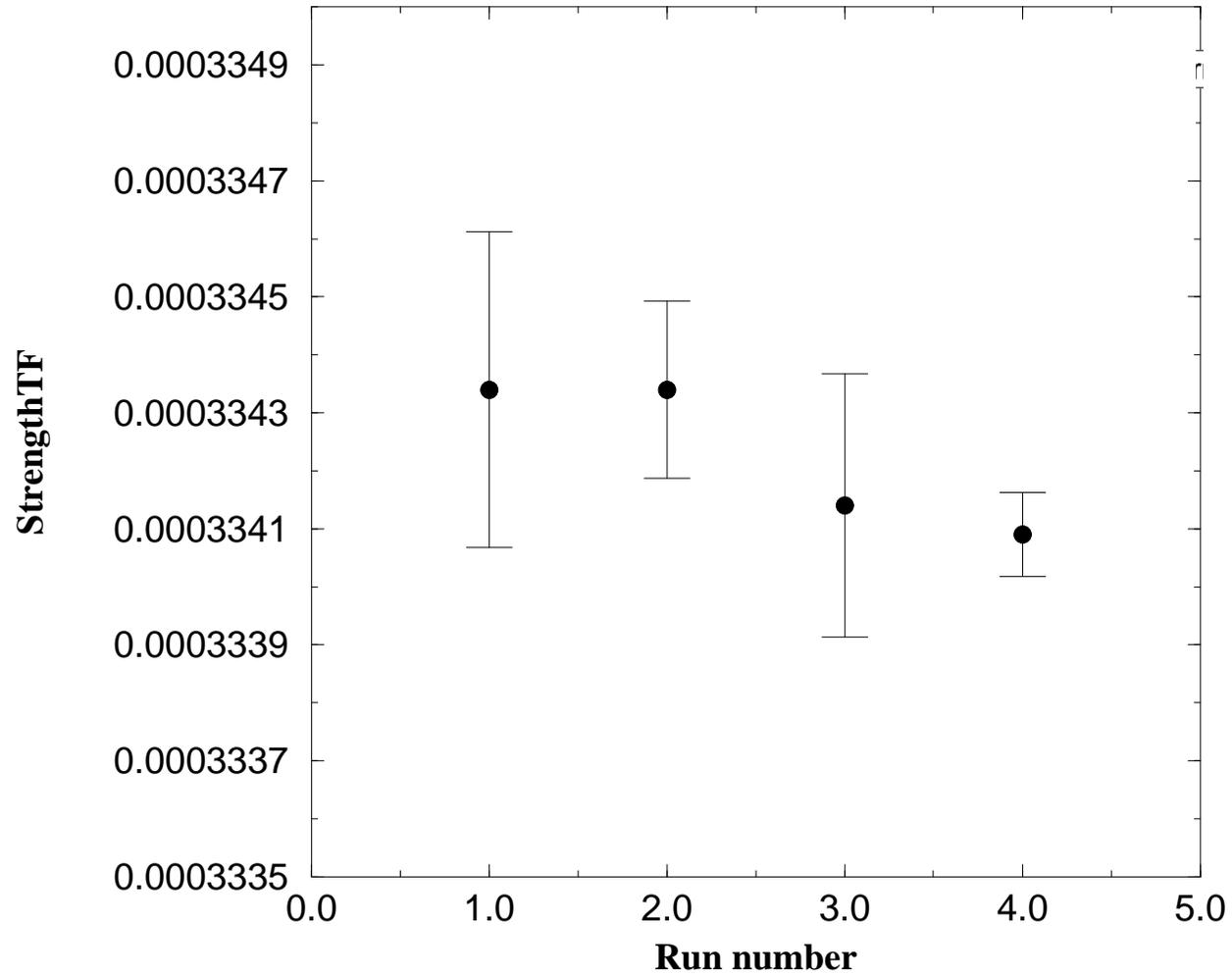


# Dipole Field Strength

4 different boards

s.d. is about 4 units.

## Field Strength for 4 Prototype Boards



Can measure quadrupole field strength with Unbucked Winding or with Dipole-Buck Winding.

## Quad Field Strength

With **DB** winding, if the bucking is nearly perfect, then the probe radius of rotation doesn't matter much - get an **absolute** measurement of quadrupole field at the level of 0.1-0.4 % **without calibration or knowledge of rotation radius**. (Can then go back and use the fact that DB quad strength = Unbucked quad strength to determine radius of rotation of unbucked winding for harmonics).

(likewise true for sextupole measurement with DQ buck winding)

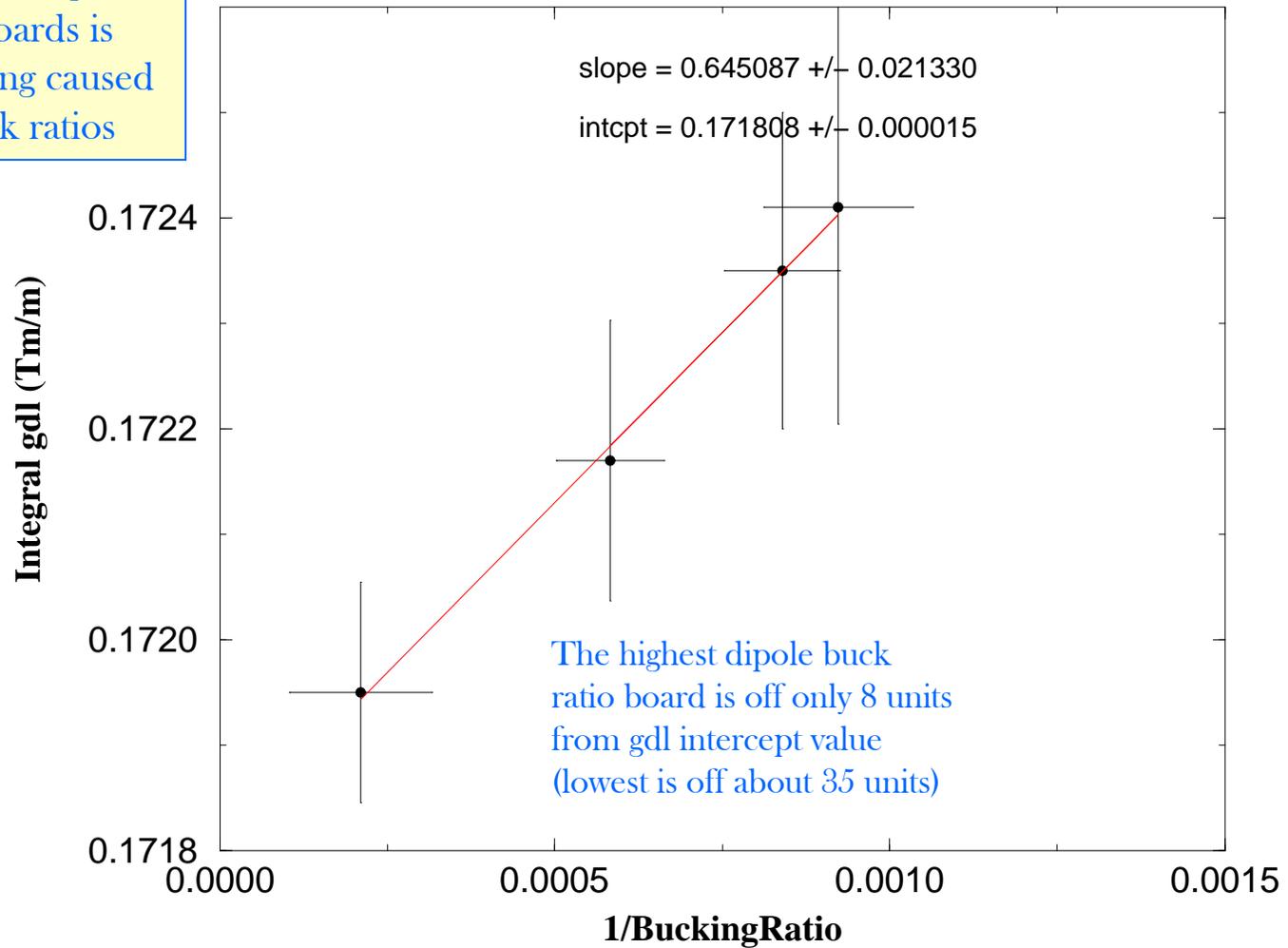
The diagram shows the equation for the measured quadrupole field strength,  $g_{meas} \approx g \left[ 1 + \frac{\bar{\varepsilon}' - \bar{\varepsilon}}{D} + \frac{1}{buckRatio} * \left( \frac{\bar{x}'}{D} + \frac{\Delta\varepsilon}{\Delta\varepsilon - \Delta\varepsilon'} \right) \right]$ , with several terms circled and annotated:

- Distance shift between loops** points to the term  $\frac{\bar{\varepsilon}' - \bar{\varepsilon}}{D}$ .
- Average radial position of UBuck loop** points to the term  $\bar{x}'$ .
- ~ 5-10 units** points to the  $buckRatio$  term.
- ~ 2 for this RBR** points to the  $buckRatio$  term.
- Bucking ratio dependent term: ~ 0 for very high buck ratio** points to the  $buckRatio$  term.
- Difference in width error of the two loops. This term is an implicit function of BR** points to the term  $\frac{\Delta\varepsilon}{\Delta\varepsilon - \Delta\varepsilon'}$ .
- $\Delta g \sim 5 \text{ units for } 5 \mu\text{m shift}$**  points to the  $\bar{\varepsilon}' - \bar{\varepsilon}$  term.
- $buckRatio * (\Delta\varepsilon - \Delta\varepsilon') = w$   
 $\Delta\varepsilon/w \approx 10 \text{ units for } 5 \mu\text{m err}$**  points to the  $\Delta\varepsilon - \Delta\varepsilon'$  term.
- If all error is in DBuck loop, this term is always 1; if all error is in UBuck loop, this term is 0. In general depends on err distribution.** points to the  $\Delta\varepsilon - \Delta\varepsilon'$  term.

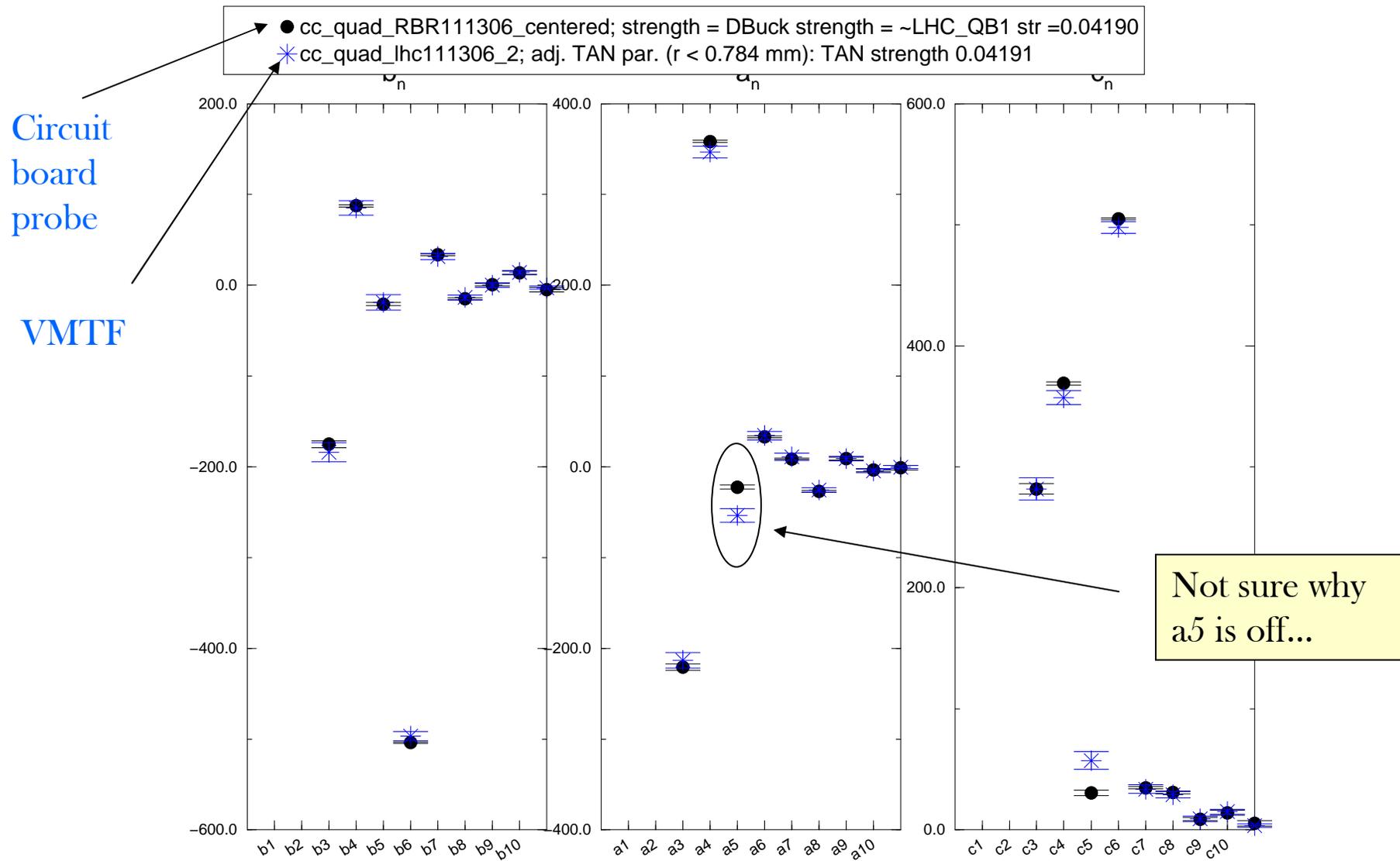
# DBuck quad strength vs buck ratio

For 4 prototype boards tested, Measured strength variation among boards is consistent with being caused by different in buck ratios

### DBuck Meas. Quad Strength vs Buck Ratio



# Harmonics of short “coffee can” magnet measured with circuit probe and VMTF tangential probe.

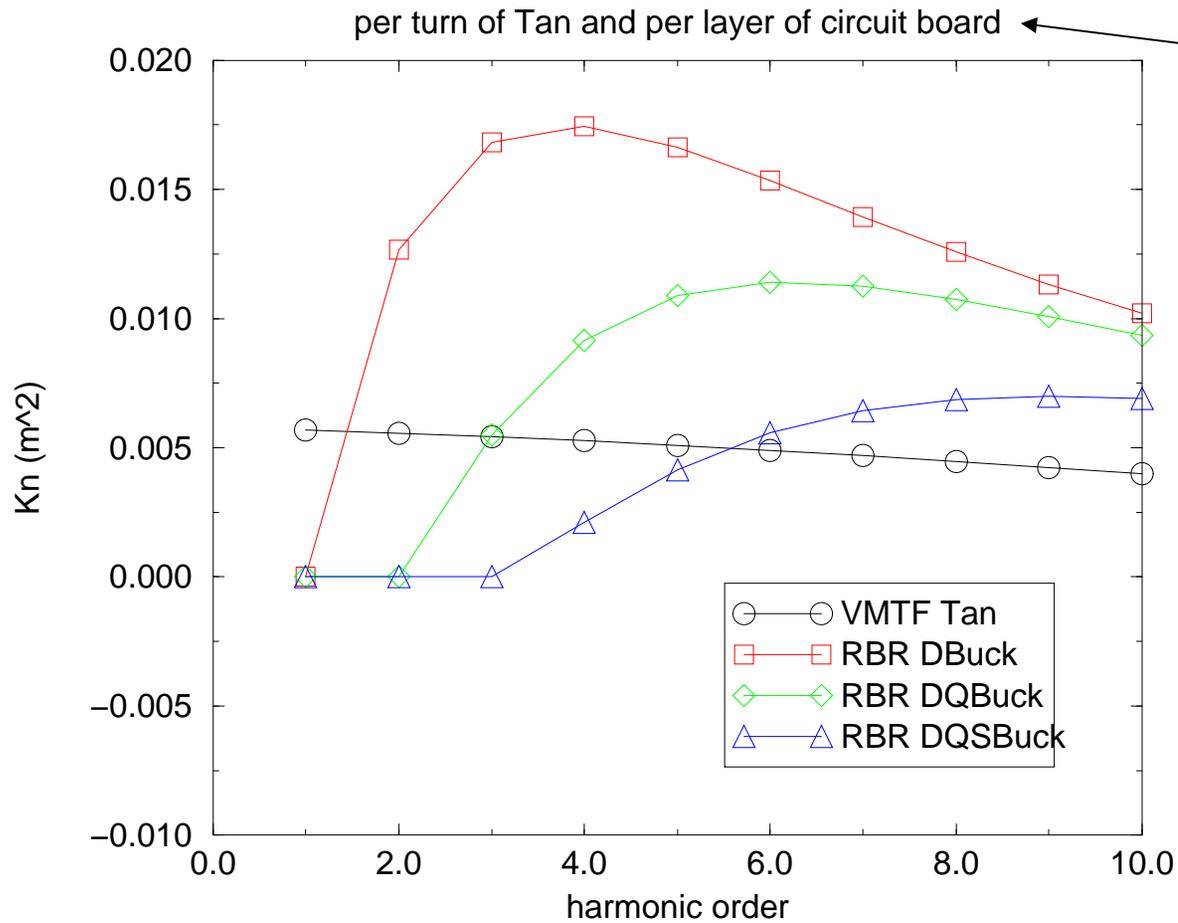


# How does Circuit probe sensitivity compare to Tangential coil for a given aperture?

- Assumptions for a generalized comparison
  - Tan has 15 deg. opening angle. Use unbucked Kn (best case)
  - Use circuit board with 4 loops, assume trace spacing is 0.25mm (0.15mm/0.1mm space/trace)
  - Fill circuit board with traces allowing 1mm in center of loops for connection vias (similar to existing probe designs)

Tangential  
vs. circuit  
board Kn  
comparison

### Sensitivity of Tan and Circuit Board Probes



Comparison made normalized to number of TAN turns and number of circuit board layers (e.g. 20 turn TAN winding compared to 20 layer circuit board)

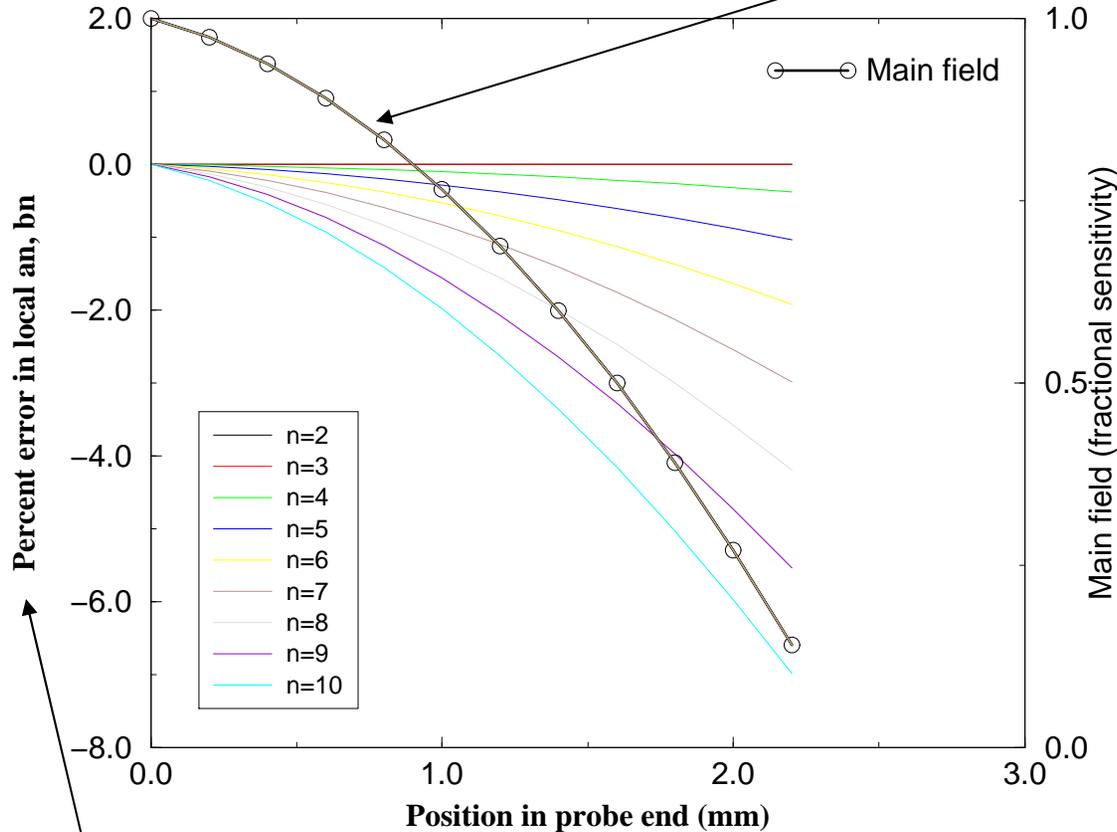
➔ Conclusion: Generally, circuit board probes will have comparable or a bit higher sensitivity for a probe of a given radius.

# Probe End Effects - strength

- Ends winding areas can be fairly short even compared to traditional probes (2-3mm end for probe with 10-15 turns per loop)
- Strength → accounted for if use exact lengths of traces when calculating sensitivity (or can use “effective length”) (effective length of end of circuit board loop is  $\sim 0.63\%$  of physical length of end).

# Harmonics end effects

**Local  $a_n, b_n$  error through RBR Probe End**  
**RBR prototype 2, DBuck winding, 15Jun06**



Strength drops through end region - can precisely calculate  $K_n$  or use effective length of probe (length it would be if it dropped as step function). (About 63% of physical length (for this prototype)).

End effects on measured harmonics are small - few percent error locally (i.e. in the 2-3mm end itself!). Though this is already small, gets further diluted since main field is decreasing through end.

Most probes are much longer than the end regions, so end effects on total harmonic integral is negligible.

Few percent of harmonic (which is at level of units to start with).

## costs

- 2 layer, 39mm: \$10
- 30 layer, 39mm (with buried vias): \$1500
- 22 layer, 1m: \$400
- 22 layer, 1.2m: \$4000
- Buried vias, layers, increase costs: to some extent also tight spacing of space/trace
- Some 'setup' fees – can be significant depending on job and company.

## notes

- Resistances can be high - (kOhms) - have to have high impedance inputs to electronics.
- Shorts can occur during production - testing/inspection needed (optical, resistance).

## conclusions

- Circuit boards can be incorporated as a tool for precision magnetic measurements.
- Can provide accurate strength of fundamental fields and higher multipoles.
- Some care needed in design and in fabrication (experienced circuit board designer and a company that you can work with help a lot).
- Compare well with tangential probes; analysis straightforward.
- Hard to push much past 1m in length.